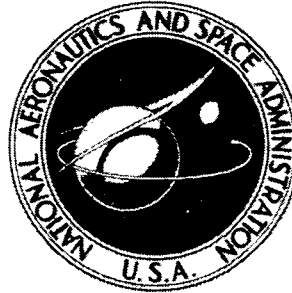


**NASA TECHNICAL
MEMORANDUM**



NASA TM X-1762

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**APPLICATION OF A MODIFIED
FAST FOURIER TRANSFORM
TO CALCULATE HUMAN OPERATOR
DESCRIBING FUNCTIONS**

by Richard S. Shirley
Electronics Research Center
Cambridge, Mass.

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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SUMMARY

A version of the fast Fourier transform (FFT) is used in a hybrid computer program to permit processing of tracking data to yield the human operator's describing function almost immediately after the period of data-taking. The use of the FFT allows the final calculation time required to process 216 seconds of tracking data to be reduced to 3 seconds from the 10 minutes previously required on the same computer. The algorithm used permits the bulk of the analysis of the data to be performed while the data are being taken, and does not require all the data to be present in core before processing begins.

TABLE OF SYMBOLS

a the index of summation for the additive portion of the FFT

A_k a constant which weights the sinusoids composing the system input, see Table I

A_{xk} the real part of the truncated Fourier transform of $x(t)$ at the frequency ω_k , given by

$$\int_0^T x(t) \cos (\omega_k t) dt$$

B_{xk} the imaginary part of the truncated Fourier transform of $x(t)$ at the frequency ω_k , given by

$$\int_0^T x(t) \sin (\omega_k t) dt$$

c a subscript referring to the output of the human operator at the control stick (see Figures 1 and 4)

$c(n\Delta t)$ the data samples taken at the human operator's output

TABLE OF SYMBOLS (cont'd)

D_k	an integer devisable by 4 used to determine the input frequencies
e	a subscript referring to the input to the human operator at the oscilloscope (see Figures 1 and 4)
$e(n\Delta t)$	the data samples taken at the human operator input
FFT	Fast Fourier Transform
$F_x(\omega_k)$	the truncated Fourier transform of $x(t)$ at the frequency ω_k , given by
$\int_0^T x(t)e^{-j\omega t} dt$	
h	a subscript used to denote frequencies between the input frequencies, equal to 1, 2, 3,...
i	a subscript referring to the system input (see Figures 1 and 4)
$i(n\Delta t)$	the system input equals
$\sum_{k=1}^{14} A_k \sin(\omega_k n\Delta t)$	
j	the square root of -1.
k	a subscript used to denote the input frequencies, equal to 1, 2, 3, ..., 14
$m(n\Delta t)$	the data samples taken at the system output
n	the index of summation for the multiplicative portion of the FFT
N	the number of data samples taken, 10,800
T	the period of data-taking, equal to 216 seconds
$Y_c(\omega)$	the dynamics of the controlled element (see Figures 1 and 4)
$Y_p(\omega)$	the linear portion of the quasi-linear describing function

β_k	$(N/D_k) - 1$
γ_k	$(D_k/4) - 1$
Δt	the time increment between interrupts, and hence the time between data samples, equals .02 sec
ω_k	the frequencies of the sinusoids comprising the system input, see Table I
ω_h	frequencies between the ω_k 's
$\Phi_{ic}(\omega)$	the cross power spectral density between the human operator's output and the system input
$\Phi_{ie}(\omega)$	the cross power spectral density between the human operator's input and the system input
$\Phi_{nn}(\omega)$	the continuous power spectral density of the human operator's remnant

INTRODUCTION

Only recently have dynamic models of the human operator been used effectively in the design of man-vehicle systems. This is due partially to a lack of understanding of the human operator and also to the difficulty and expense of experimentally determining values for the various parameters of existing models. Improvements in computers and computational techniques are overcoming these difficulties, and already it is possible to bring about significant improvements in a man-vehicle system through the use of pilot models in preliminary design (refs. 1 and 2). This paper describes a computational technique which reduces greatly the cost of obtaining values permitting the use of a current pilot model, i.e., the quasi-linear describing function.

One way to characterize the behavior of a human operator in a continuous tracking task is by a quasi-linear describing function, which consists of a linear describing function and a remnant. The linear describing function is the average frequency response of the human operator, i.e., his amplitude ratio and phase as a function of frequency. The remnant, characterized by a continuous power spectral density, is that portion of the human operator's output which is not linearly correlated with his input. The total output of the human operator is the sum of the remnant and the output of the linear describing function* (see Figure 1).

*Examples of human operator describing functions are shown in Figures 2 and 3.

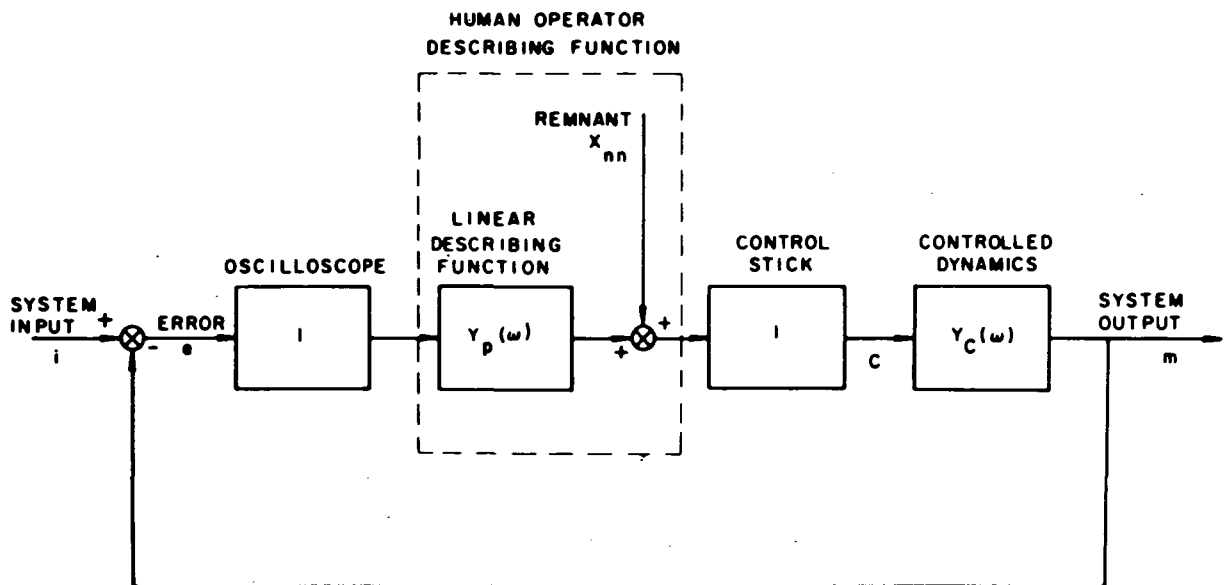


Figure 1.- Block diagram of the human operator in a compensatory tracking system.

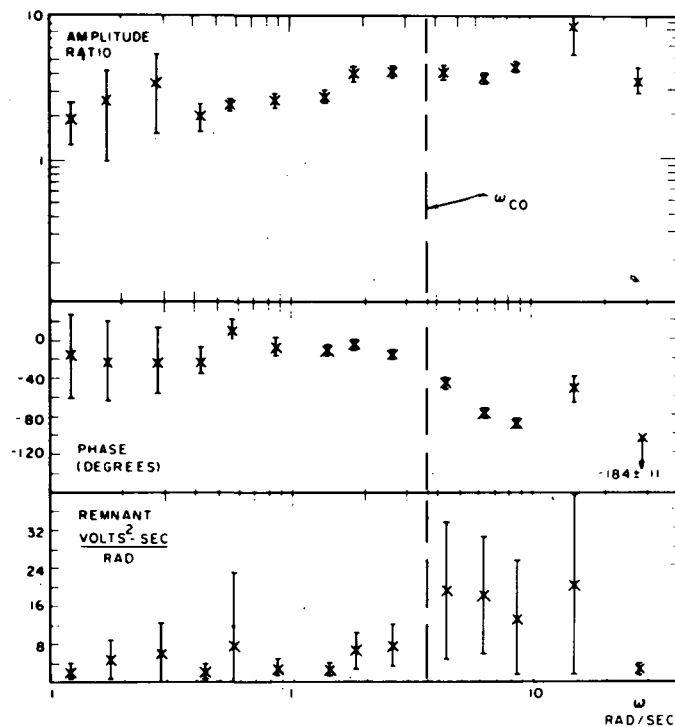


Figure 2.- $Y_p(\omega)$ measured for $Y_c(s) = 1/s$

A direct way to measure describing functions in the laboratory involves the use of a hybrid computer and the method of Fourier coefficients. The method of Fourier coefficients has been extensively investigated and is described in detail (ref. 3). It will be briefly outlined here for completeness. The human operator is placed in a control loop, possibly as shown in Figures 1 and 4. The system input, a sum of sinusoids of known amplitude, phase, and frequency is updated every Δt seconds; simultaneously, data are taken at the human operator's input and output. At the end of T seconds, the sampled values of the human operator's input and output are processed as follows:

$$A_{ck} = \frac{\Delta t}{T} \sum_{n=1}^N c(n\Delta t) \cos(\omega_k n\Delta t) \quad (1)$$

$$B_{ck} = \frac{\Delta t}{T} \sum_{n=1}^N c(n\Delta t) \sin(\omega_k n\Delta t) \quad (2)$$

$$A_{ek} = \frac{\Delta t}{T} \sum_{n=1}^N e(n\Delta t) \cos(\omega_k n\Delta t) \quad (3)$$

$$B_{ek} = \frac{\Delta t}{T} \sum_{n=1}^N e(n\Delta t) \sin(\omega_k n\Delta t) \quad (4)$$

$$F_c(\omega_k) = A_{ck} - jB_{ck} \quad (5)$$

$$F_e(\omega_k) = A_{ek} - jB_{ek} \quad (6)$$

$$Y_p(\omega_k) = \frac{F_c(\omega_k)}{F_e(\omega_k)} \quad (7)$$

$$\angle Y_p(\omega_k) = -\tan^{-1} \frac{B_{ck}}{A_{ck}} + \tan^{-1} \frac{B_{ek}}{A_{ek}} \quad (8)$$

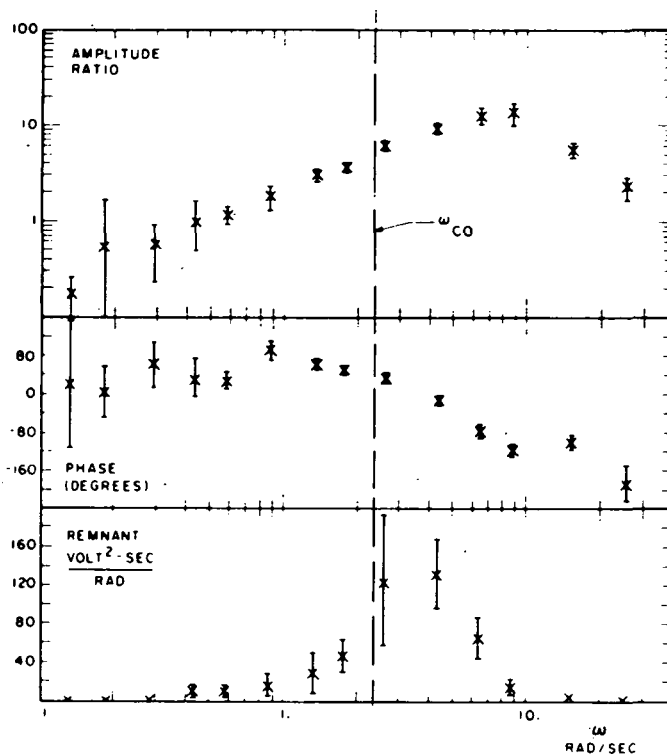


Figure 3.- $Y_p(\omega)$ measured for $Y_c(s) = 1/s^2$

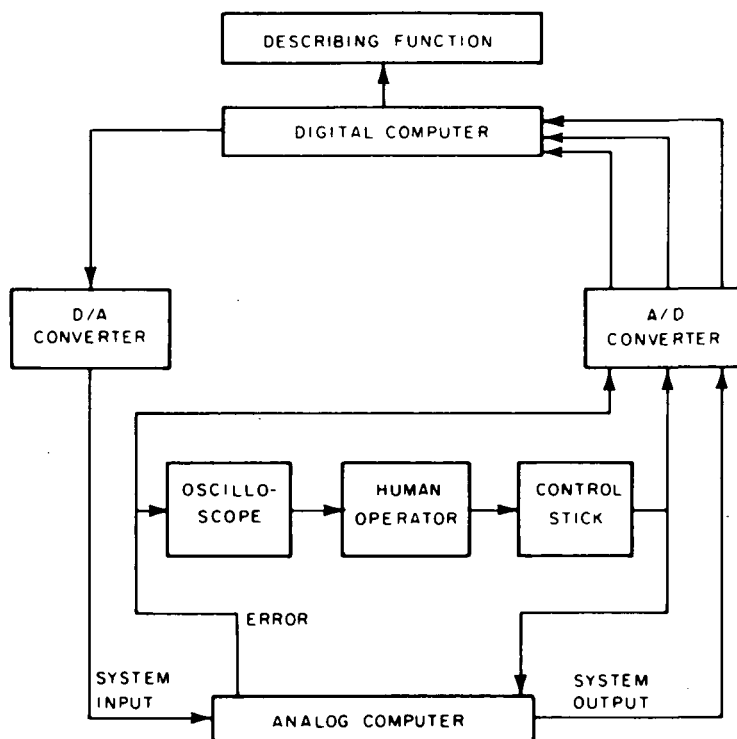


Figure 4.- Flow diagram of the human operator in a compensatory tracking system.

$$|Y_p(\omega_k)| = \left[\frac{A_{ck}^2 + B_{ck}^2}{A_{ek}^2 + B_{ek}^2} \right]^{1/2} \quad (9)$$

$$\Phi_{cc}(\omega_h) = \frac{1}{2\pi T} |F_c(\omega_h)|^2 \quad (10)$$

$$\Phi_{nn}(\omega_h) = \Phi_{cc}(\omega_h) |1 + Y_p Y_c(\omega_h)|^2 \quad (11)$$

where the ω_k 's are the input frequencies, and the ω_h 's lie between the ω_k 's.

This paper describes how a version of the fast Fourier transform (FFT) is used to compute human operator describing functions, or more specifically, how a version of the FFT is used to solve Eqs. (1) through (4), while the data samples, $c(n\Delta t)$ and $e(n\Delta t)$, are being taken. The FFT is an algorithm which greatly reduces the time required to calculate the truncated Fourier transform, or periodogram, of a sampled time signal. The savings are obtained by replacing calculations which involve trigonometric functions or multiplications with simple additions. The replacement is accomplished by taking advantage of the symmetries of the sine and cosine functions, and by further taking advantage of relationships between the frequencies at which the Fourier analysis is performed.

THE VERSION OF THE FFT USED

The version of the FFT used takes advantage only of the symmetries of the sine and cosine functions. It does not take advantage of the relationships among the frequencies at which the Fourier analysis is performed. By not using the complete version of the FFT, it becomes possible to perform the bulk of the data-processing during the Δt seconds between interrupts while the experiment is still in process. The requirement that the data be in core before processing, or even that the data fit in core, is avoided. The following derivation of the algorithm used will make this point clearer. It should be noted that before the FFT was used it was not possible to perform the calculations between interrupts because the computation time required was over two and a half times greater than that which was available.

It is desired to evaluate Eqs. (1) through (4) using a digital computer. In order to permit the use of the FFT, the input frequencies, ω_k , will be restricted to

$$\omega_k = \frac{2\pi}{D_k \Delta t}$$

where the D_k are chosen from 4, 8, 12, 16, etc. The method of Fourier coefficients further requires that the ratio N/D_k be an integer (where N is the number of data samples taken at intervals Δt). The derivation for A_{ek} and B_{ek} is identical to the derivation which follows for A_{ck} and B_{ck} .

Using the identities

$$\begin{aligned}\sin(\theta + 2\pi) &= \sin \theta, \text{ and} \\ \cos(\theta + 2\pi) &= \cos \theta\end{aligned}$$

or

$$\left. \begin{aligned}\sin(\omega_k \Delta t) &= \sin \left[(aD_k + 1) \omega_k \Delta t \right] \\ \cos(\omega_k \Delta t) &= \cos \left[(aD_k + 1) \omega_k \Delta t \right]\end{aligned} \right\} \quad a = 0, 1, 2, 3, \dots$$

permits Eqs. (1) and (2) to be rewritten as

$$A_{ck} = \frac{\Delta t}{T} \sum_{n=1}^{D_k} \left[\cos(\omega_k n \Delta t) \sum_{a=0}^{\beta_k} c \left[\Delta t (n + aD_k) \right] \right] \quad (12)$$

$$B_{ck} = \frac{\Delta t}{T} \sum_{n=1}^{D_k} \left[\sin(\omega_k n \Delta t) \sum_{a=0}^{\beta_k} c \left[\Delta t (n + aD_k) \right] \right] \quad (13)$$

where $\beta_k = (N/D_k) - 1$. The identities

$$\begin{aligned}\sin(\theta - \pi) &= -\sin \theta, \text{ and} \\ \cos(\theta - \pi) &= \cos \theta\end{aligned}$$

or

$$\sin \left[\omega_k \Delta t \left(n - \frac{D_k}{2} \right) \right] = -\sin (\omega_k n \Delta t)$$

$$\cos \left[\omega_k \Delta t \left(n - \frac{D_k}{2} \right) \right] = \cos (\omega_k n \Delta t)$$

permit Eqs. (12) and (13) to be written as

$$A_{ck} = \frac{\Delta t}{T} \sum_{n=1}^{D_k/2} \left[\cos (\omega_k n \Delta t) \sum_{a=0}^{\beta_k} \left\{ c [\Delta t (n + a D_k)] - c \left[\Delta t \left(n + \frac{D_k}{2} + a D_k \right) \right] \right\} \right] \quad (14)$$

$$B_{ck} = \frac{\Delta t}{T} \sum_{n=1}^{D_k/2} \left[\sin (\omega_k n \Delta t) \sum_{a=0}^{\beta_k} \left\{ c [\Delta t (n + a D_k)] - c \left[\Delta t \left(n + \frac{D_k}{2} + a D_k \right) \right] \right\} \right] \quad (15)$$

Finally, the identities $\sin (-\theta) = -\sin \theta$, $\cos (-\theta) = \cos \theta$, $\sin (\pi/2) = \cos (\pi) = 1$, and $\sin (\pi) = \cos (\pi/2) = 0$ permit Eqs. (14) and (15) to be written as

$$A_{ck} = \frac{\Delta t}{T} \sum_{n=1}^{\gamma_k} \left[\cos (\omega_k n \Delta t) \sum_{a=0}^{\beta_k} \left\{ c [\Delta t (n + a D_k)] - c \left[\Delta t \left(n + \frac{D_k}{2} + a D_k \right) \right] - c \left[\Delta t \left(\frac{D_k}{2} - n + a D_k \right) \right] + c \left[\Delta t \left(\frac{D_k}{2} - n + \frac{D_k}{2} + a D_k \right) \right] \right\} \right. \\ \left. - \frac{\Delta t}{T} \sum_{a=0}^{\beta_k} \left\{ c \left[\Delta t \left(\frac{D_k}{2} + a D_k \right) \right] - c \left[\Delta t \left(\frac{D_k}{2} + \frac{D_k}{2} + a D_k \right) \right] \right\} \right] \quad (16)$$

$$\begin{aligned}
B_{ck} = & \frac{\Delta t}{T} \left[\sum_{n=1}^{\gamma_k} \sin(\omega_k n \Delta t) \sum_{a=0}^{\beta_k} \left\{ c \left[\Delta t \left(n + a D_k \right) \right] - c \left[\Delta t \left(n + \frac{D_k}{2} + a D_k \right) \right] \right. \right. \\
& + c \left[\Delta t \left(\frac{D_k}{2} - n + a D_k \right) \right] - c \left[\Delta t \left(\frac{D_k}{2} - n + \frac{D_k}{2} + a D_k \right) \right] \left. \right\} \\
& + \frac{\Delta t}{T} \sum_{a=0}^{\beta_k} \left\{ c \left[\Delta t \left(\frac{D_k}{4} + a D_k \right) \right] - c \left[\Delta t \left(\frac{D_k}{4} + \frac{D_k}{2} + a D_k \right) \right] \right\} \quad (17)
\end{aligned}$$

where $\gamma_k = (D_k/4) - 1$. Equations (16) and (17) represent the algorithm used in the hybrid program. The summation over "a" is performed between interrupts during the experiment and is called the "additive portion" of the FFT. At the end of the data-taking period, the summation over n (called the "multiplicative portion" of the FFT) and the calculation of the human operator's describing function [using Eqs. (8) and (9)], can be performed in less than three seconds.

The hybrid computer program is written in a Fortran IV language which includes hybrid commands. The program is listed in Appendix A. Table I lists the values of the experimental parameters, including those which characterize the system input. Figure 5 is a flow diagram of the additive portion of the FFT. Figure 6 shows a flow diagram of the hybrid program, and lists the time taken by each part of the program, both for the FFT version and for the version written the old way [directly computing Eqs. (1) through (4)]. As shown in Figure 6, the FFT permits a saving of nearly ten minutes per run, effectively reducing the run time to the time required to take the data and print the results.

RESULTS

An initial check of the hybrid program was made by taking measurements across known filters. The results shown in Figures 7 and 8 are quite accurate, and are repeatable.

Measurements were then taken of the author's tracking performance in a control loop, as shown in Figures 1 and 4. Ten runs were made with each of the controlled elements, $1/s$ and $1/s^2$. The describing functions shown in Figures 2 and 3 are comparable with established results (ref. 3).

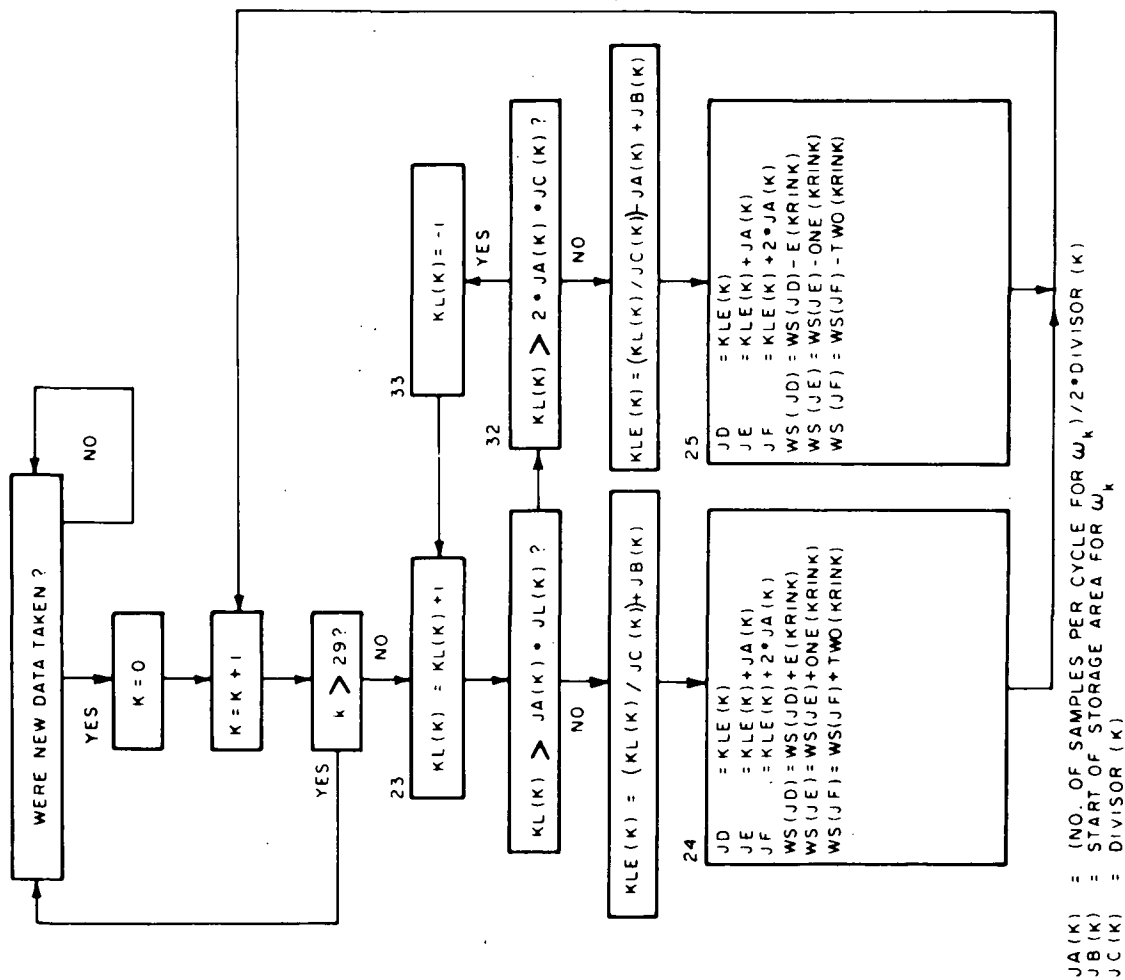
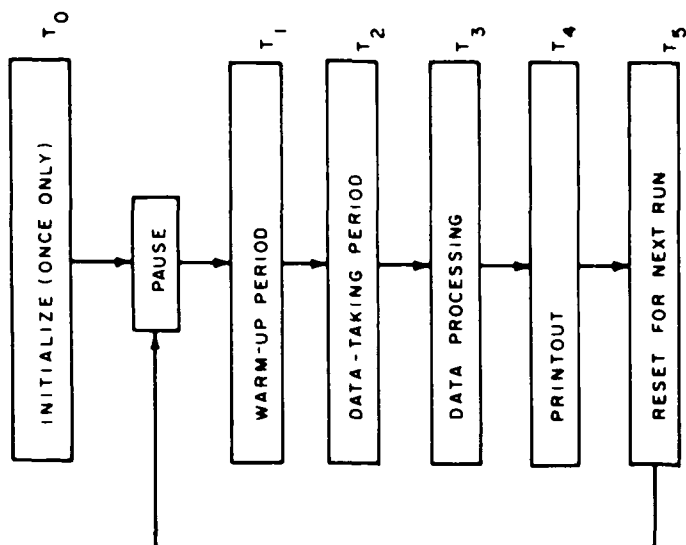


Figure 5.- Flow chart for additive portion of FFT



	WITHOUT FFT	WITH FFT	
T_0	180	180	ONCE ONLY INITIALIZATION
T_1	24	24	EXPERIMENT RUNNING
T_2	216	216	
T_3	600	3	PROCESS DATA 8
T_4	5	5	PRINT DATA 8
T_5	15	15	RESET
	860 SECS	263 SECS	TOTAL (EXCEPT T_0)

Figure 6.- Flow diagram and times for computer runs

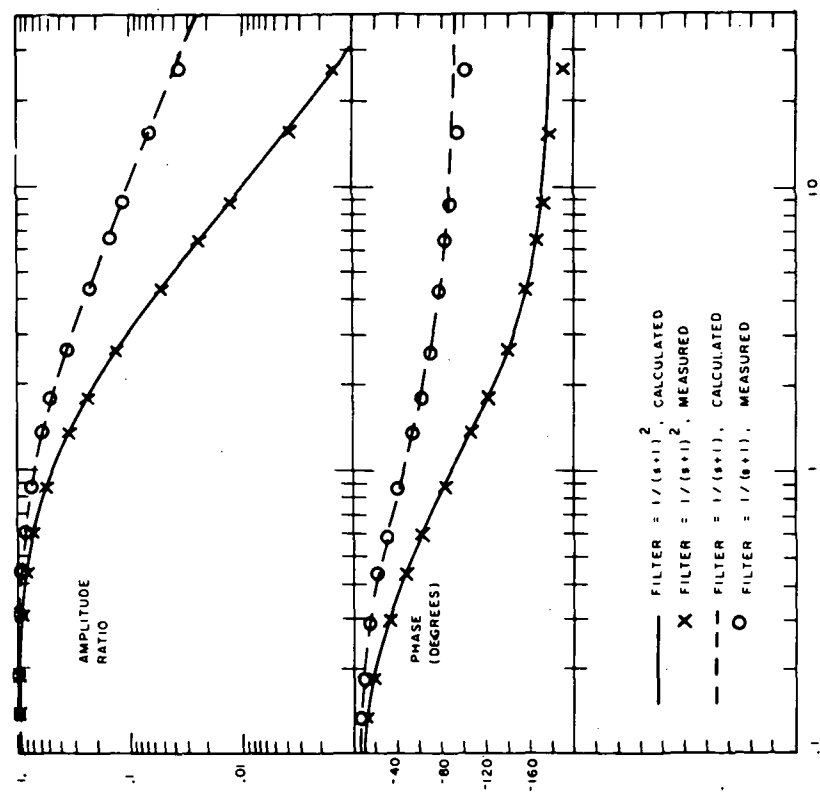


Figure 7.- Measurement of a known filter

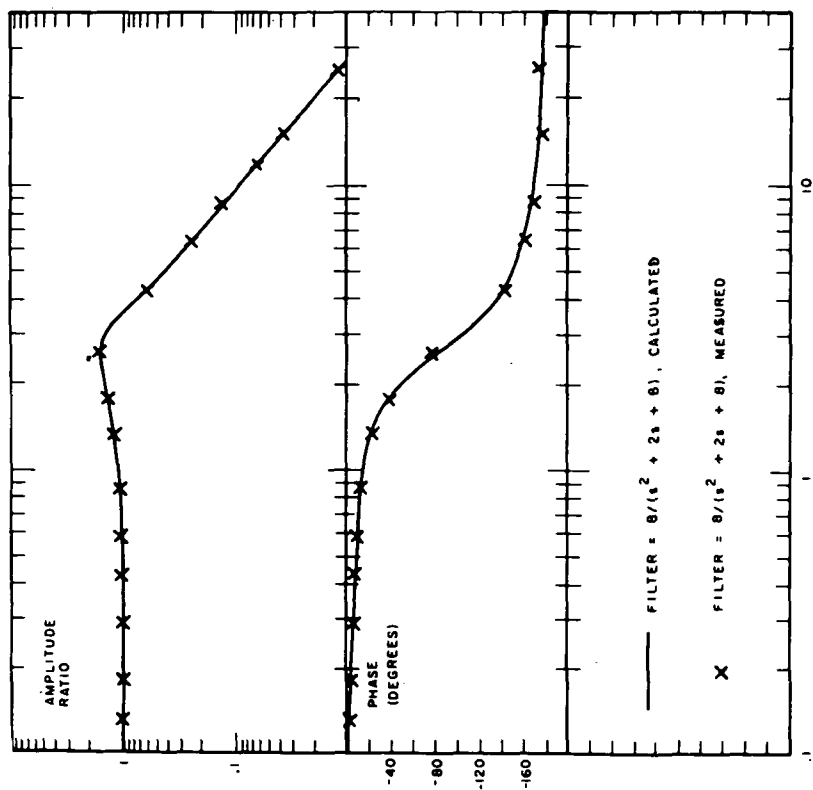


Figure 8.- Measurement of a known filter

TABLE I

PARAMETER VALUES USED FOR THE HYBRID PROGRAM

k	A _k volts	ω _k rad/sec	k	A _k volts	ω _k rad/sec
1	.2	26.18	8	-1.	1.309
2	- .2	15.71	9	1.	.8727
3	.2	8.727	10	-1.	.5818
4	- .2	6.545	11	1.	.4363
5	.2	4.363	12	-1.	.2909
6	-1.	2.618	13	1.	.1745
7	1.	1.745	14	-1.	.1164

Δt = time between interrupts = .02 sec

T_1 = warm-up time before data-taking = 24 sec

T = period of data-taking = 216 sec

$$i(n\Delta t) = \text{system input} = \sum_{k=1}^{14} A_k \sin(\omega_k n\Delta t)$$

No comparison is made between results for the programs with and without the FFT (on Figures 2, 3, 7, 8) because the results are identical, as is shown analytically in the derivation of Eqs. (16) and (17). The comparison between the computation times for the two programs (Figure 6) however, indicates the substantial savings obtained by using the FFT. The only penalty paid for the reduced computational time is an increase in the complexity of the written Fortran program, as shown in Appendix A.

National Aeronautics and Space Administration
 Electronics Research Center
 Cambridge, Massachusetts, November 1968
 125-19-01-11-25

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2. Elkind, J. I., et al.: An Optimal Control Method for Predicting Control Characteristics and Display Requirements for Manned-Vehicle Systems. AFFDL-TR-67-187, Apr. 1968.
3. McRuer, D. T., et al.: Human Pilot Dynamics in Compensatory Systems. AFFDL-TR-65-15, July 1965.
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National Aeronautics and Space Administration
Electronics Research Center
Cambridge, Massachusetts, December, 1968
125-19-01-11-25

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108 FORMAT(///,4X,1HK,6X,8HFREQ.(K),7X,7HREM1(K),8X,7HREM2(K),//,

I(15,3E15.4))

109 FORMAT (10X,3I10)

110 FORMAT (///,4X,5HJA(K),4X,5HJB(K),4X,5HJC(K),//,(2X,15,4X,15,4X,15)

1)

111 FORMAT (1H1,/,4X,1HK,5X,4HW(K),//,(15,2E15.4))

112 FORMAT (///,4X,23HREMNANT POWER AT ONE = ,1E15.4,/,4X,

123HREMNANT POWER AT TWO = ,1E15.4)

113 FORMAT (///,4X,1HK,6X,8HFREQ.(K),7X,8HREMA1(K),7X,8HREMA2(K),//,

I(15,3E15.4))

114 FORMAT (///,10X,\$THE FOLLOWING REMNANT VALUES ARE CORRECTED FOR TH

1E LOOP GAINS,/, \$I.E., PHI ACTUAL = PHI MEAS. TIMES I + YPYC SQUARE
2D\$)

115 FORMAT (6E10.4)

116 FORMAT (/,4X,8HCONS2 = ,1E15.4)

117 FORMAT (///,4X,7HXISQ = ,1E15.4,10X,7HXZSQ = ,1E15.4)

C

C DIMENSION STATEMENTS

COMMON PUT(1080),E(1080),ONE(1080),TWO(1080),KONK,LOP,KANK,

IN,M,MO,KRINK,PUSQ,ERRSQ,ONESQ,TWOSQ

COMMON JA(29),JB(29),JC(29),WS(4300),KL(29),KLE(29)

DIMENSION W(30),AE(15),BE(15),AI(15),BI(15),A2(15),B2(15),

1AREM1(15),BREM1(15),AREM2(15),BREM2(15)

DIMENSION AR1(15),AR2(15),PHA1(15),PHA2(15),REM1(15),REM2(15)

DIMENSION AM(15)

DIMENSION REMA1(15),REMA2(15)

C

C

C THE PROGRAM CAN BE RECALLED TO THIS POINT BY IFINITIA AT ANY TIME

C BY HITTING INTERRUPT 33 AND TYPING A CARRIAGE RETURN

CALL IFINITIA

C

C

C CONNECT THE CONSOLE

S

EOM 031120

C

C

C PUT THE ANALOG COMPUTER INTO IC MODE

CALL IC

C

C

C SENSE SWITCH4 DETERMINES IF REWIND 3 OR NOT

IF (SENSE SWITCH4) 98,99

99 REWIND 3

98 CONTINUE

C

C

C SENSE SWITCH1 DETERMINES IF FREQUENCY AND REGISTER VALUE CARDS ARE

C

READ

IF (SENSE SWITCH1) 23,24

C

C

C SENSE SWITCH2 DETERMINES IF INPUT CALCULATED

23 IF (SENSE SWITCH2) 17,26

C

C

C READ IN 29 FREQUENCIES IN ORDER, HIGH FREQUENCIES FIRST,

C

C IN RADIANS/SECOND, STARTING WITH A REMNANT FREQUENCY AND ALTERNA-

C

C TING THEREAFTER WITH THE INPUT FREQUENCIES. THE FREQUENCIES MUST

C

C ALL BE INTEGER MULTIPLES OF $2(\pi)/\text{RUNTIME}$, AND THE NUMBER OF

C

C SECONDS PER CYCLE MUST EQUAL $4I(\Delta)$, WHERE I IS AN INTEGER AND

C

C Δ IS THE TIME BETWEEN DATA POINTS.

24 READ(5,102) (W(K),K=1,29)

```

C      WRITE(6,111) (K,W(K),K=1,29)
C
C      READ IN THE REGISTER VALUES FOR THE ADDITIVE PART OF THE FFT
C      READ(5,109) (JA(K),JB(K),JC(K),K=1,29)
C      WRITE(6,110) (JA(K),JB(K),JC(K),K=1,29)
C
C      INPUT (CALCULATED EVERY DELT)
C      CONS1 SCALES THE INPUT
C      26 CONS1=9.5
C      REWIND INPUT TAPE PRIOR TO STORING INPUT
C      REWIND 1
C      ONW SETS THE STARTING TIME FOR THE INPUT, AND IS NEGATIVE
C      SO THAT THE HUMAN OPERATOR IS IN A STEADY-STATE TRACKING
C      CONDITION WHEN THE ONSET OF DATA-TAKING OCCURS
C      ONW=-1080.
C      DELT IS THE TIME INCREMENT BETWEEN INPUT VALUES, AND MUST EQUAL
C      DELTA, THE TIME INCREMENT BETWEEN DATA POINTS.
C      DELT=.02
C      THE AM(K) SCALE THE INPUT SINUSOIDS
C      AM(1)=.2
C      AM(2)=-.2
C      AM(3)=.2
C      AM(4)=-.2
C      AM(5)=.2
C      AM(6)=-1.
C      AM(7)=1.
C      AM(8)=-1.
C      AM(9)=1.
C      AM(10)=-1.
C      AM(11)=1.
C      AM(12)=-1.
C      AM(13)=1.
C      AM(14)=-1.
C      AM(15)=1.
C
C      THE INPUT IS CALCULATED IN BLOCKS OF 540 VALUES AND STORED ON
C      MAGNETIC TAPE (UNIT 1).
C      DO 19 J=1,30
C      DO 1 K=1,540
C      PUT(K)=0.
C      ONW=ONW+1.
C      T=ONW*DELT
C      DO 20 L=1,14
C      PUT(K)=PUT(K)+AM(L)*SIN(T*W(2*L))
C      20 CONTINUE
C      PUT(K)=CONS1*PUT(K)
C      1 CONTINUE
C      M=1
C      N=540
C      CALL BUFFEROUT(1,1,PUT(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      19 CONTINUE
C
C
C      17 CONTINUE
C      THE INTERRUPT IS CONNECTED, BUT NOT ENABLED

```

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CONNECT (40,INTR)
EOM 020020
POT =00700000

INITIALIZE FOR THE RUN

ZERO THE BUFFER AREAS

DO 92 K=1,1080

PUT(K)=0.

E(K)=0.

ONE(K)=0.

TWO(K)=0.

92 CONTINUE

ZERO THE DATA TAPE

REWIND 2

DO 91 K=1,90

N=540

M=1

CALL BUFFEROUT(2,1,E(M),2*(N-M+1),ISTATUS)

CALL GOTO(ISTATUS)

91 CONTINUE

THE MAGNETIC TAPE UNITS ARE INITIALIZED, UNIT 1 FOR THE INPUT,
AND UNIT 2 FOR THE DATA.

REWIND 1

REWIND 2

ZERO THE REGISTERS WHERE THE FOURIER COEFFICIENTS ARE TO
BE CALCULATED.

DO 31 K=1,15

AE(K)=0.

BE(K)=0.

A1(K)=0.

B1(K)=0.

A2(K)=0.

B2(K)=0.

AREM1(K)=0.

BREM1(K)=0.

AREM2(K)=0.

BREM2(K)=0.

31 CONTINUE

INITIALIZE FOR THE ADDITIVE PART OF THE FFT

DO 10 NOW=1,29

KL(NOW)=-1

10 CONTINUE

DO 14 NOW=1,4300

WS(NOW)=0.

14 CONTINUE

INITIALIZE THE COUNTERS FOR THE RUN

KRINK IS A COUNTER TO DETERMINE THE LOCATION FROM WHICH THE
NEXT INPUT VALUE SHOULD BE TAKEN FROM

KRINK=0

KONK COUNTS THE INTERRUPTS, DETERMINES WHEN THE ONSET OF DATA-

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```

C   TAKING SHOULD OCCUR, AND WHEN DATA-TAKING IS COMPLETED.
C   KONK=0
C   KANK IS THE HALF REGISTER COUNTER, 1 TO 540
C   KANK=0
C   MO DETERMINES WHICH HALF OF THE INPUT BUFFER IS BEING USED
C   MO=0
C   B IS A COUNTER ON THE DATA USED DURING THE DATA-PROCESSING
C   B=-1.
C   LOP IS THE FLAG SET BY INTR TO END DATA-TAKING
C   LOP=0
C   PUTSQ AND ERRSQ ARE THE INTEGRAL SQUARE INPUT AND ERROR
C   PUTSQ=0.
C   ERRSQ=0.
C   ONESQ=0.
C   TWOSQ=0.
C   X1SQ=0.
C   X2SQ=0.
C
C   INITIALIZE INPUT BUFFER FOR THE RUN, I.E., FILL BOTH HALVES
C   WITH INPUT VALUES
C   M=1
C   N=540
C   CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)
C   CALL GOTO(ISTATUS)
C   M=541
C   N=1080
C   CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)
C   CALL GOTO(ISTATUS)
C
C   WAIT TO START RUN ON SIGNAL FROM THE OPERATOR
C   PAUSE
C
C
C   511 CONTINUE
S   SKS 030000
S   ORU 5135
/   GO TO 511
C   513 CONTINUE
C   PUT THE ANALOG COMPUTER INTO COMPUTE MODE
C   CALL COMPUTE
C
C   ENABLE THE INTERRUPT
S   EOM 031032
C
C
C   11 CONTINUE
C   CHECK TO SEE IF IT IS THE END OF DATA-TAKING
C   IF (LOP.EQ.1) GO TO 2
C   IT IS NOT THE END OF DATA TAKING, WAIT FOR INTERRUPT
C   GO TO 11
C
C
C   IT IS THE END OF DATA TAKING, GO ON
C   2 CONTINUE
C   TURN OFF THE INTERRUPT
S   EOM 031033
C   PUT THE ANALOG COMPUTER INTO THE HOLD MODE

```

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```

C      CALL HOLD
C      TAKE THE INTEGRAL SQUARE MEASURES
C      CALL ADL(4,PUTSQ,ERRSQ,ONESQ,TWOSQ,X1SQ,X2SQ)
C      PUT THE ANALOG COMPUTER INTO IC MODE
C      CALL IC
C
C      SENSE SWITCH3 DETERMINES WHETHER TO PROCESS THE DATA AND TYPE
C      THE RESULTS, OR WHETHER TO RE-INITIALIZE FOR THE NEXT RUN
C      IF (SENSE SWITCH3) 17,22
C
C      DATA PROCESSING IS DESIRED, GO ON
C      22 CONTINUE
C      THE FOLLOWING SAVES THE LAST 540 DATA POINTS
C      N=1080
C      M=541
C      CALL BUFFEROUT(2,1,E(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      CALL BUFFEROUT(2,1,ONE(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      CALL BUFFEROUT(2,1,TWO(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C
C      THE FOLLOWING PERMITS A TOTAL OR PARTIAL TAPE DUMP
C      IF (SENSE SWITCH5) 89,90
C      89 REWIND 1
C      REWIND 2
C      N=540
C      M=1
C      CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      N=1080
C      M=541
C      CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      WRITE(6,106) (J,PUT(J),J=1,1080)
C      GO PAST THE INITIAL SPURIOUS DATA POINTS (CAUSED BY INTERRUPT
C      ROUTINE).
C      M=1
C      N=540
C      DO 16 J=1,3
C      CALL BUFFERIN(2,1,E(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      16 CONTINUE
C      NO DETERMINES EXTENT OF THE DUMP
C      NO=3
C      DO 88 K=1,NO
C      CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      CALL BUFFERIN(2,1,E(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      CALL BUFFERIN(2,1,ONE(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      CALL BUFFERIN(2,1,TWO(M),2*(N-M+1),ISTATUS)
C      CALL GOTO(ISTATUS)
C      L=(K-1)*540

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WRITE(6,105) ((L+J),PUT(J),E(J),ONE(J),TWO(J),J=1,540)

88 CONTINUE

90 CONTINUE

PROCESS THE DATA FOR 10,800 POINTS

MULTIPLICATIVE PART OF THE FFT USED TO CALCULATE THE FOURIER
COEFFICIENTS

CALCULATE THE FOURIER COEFFICIENTS FOR THE REMNANT

DEZ=3.1415927

DO 21 K=1,29,2

NE=(K+1)/2

LEB1=JB(K)+JA(K)-1

LEE1=JB(K)+2*JA(K)-1

LEB2=JB(K)+2*JA(K)-1

LEE2=JB(K)+3*JA(K)-1

LEM1=LEE1-JA(K)/2

LEM2=LEE2-JA(K)/2

AREM1(NE)=0.

AREM2(NE)=0.

BREM1(NE)=0.

BREM2(NE)=0.

JST=(JA(K)/2)-1

DO 27 JI=1,JST

VOU=FLOAT(JI)

YOU=FLOAT(JA(K))

TOU=YOU/VOU

SINUS=SIN(DEZ*TOU)

COSUS=SQRT(1.-SINUS**2.)

AREM1(NE)=AREM1(NE)+(WS(LEB1+JI)+WS(LEE1-JI))*SINUS

AREM2(NE)=AREM2(NE)+(WS(LEB2+JI)+WS(LEE2-JI))*SINUS

BREM1(NE)=BREM1(NE)+(WS(LEB1+JI)-WS(LEE1-JI))*COSUS

BREM2(NE)=BREM2(NE)+(WS(LEB2+JI)-WS(LEE2-JI))*COSUS

27 CONTINUE

AREM1(NE)=AREM1(NE)+WS(LEM1)

AREM2(NE)=AREM2(NE)+WS(LEM2)

BREM1(NE)=BREM1(NE)-WS(LEE1)

BREM2(NE)=BREM2(NE)-WS(LEE2)

21 CONTINUE

CALCULATE THE FOURIER COEFFICIENTS FOR THE DESCRIBING FUNCTION

DO 28 K=2,28,2

NE=K/2

LEBE=JB(K)-1

LEEE=JB(K)+JA(K)-1

LEB1=JB(K)+JA(K)-1

LEE1=JB(K)+2*JA(K)-1

LEB2=JB(K)+2*JA(K)-1

LEE2=JB(K)+3*JA(K)-1

LEME=LEEE-JA(K)/2

LEM1=LEE1-JA(K)/2

LEM2=LEE2-JA(K)/2

AE(NE)=0.

BE(NE)=0.

A1(NE)=0.

B1(NE)=0.

A2(NE)=0.

B2(NE)=0.

JST=(JA(K)/2)-1

DO 29 JI=1,JST

VOU=FLOAT(JI)

VOU=FLOAT(JA(K))

TOU=VOU/VOU

SINUS=SIN(DEZ*TOU)

COSUS=SQRT(1.-SINUS**2.)

AE(NE)=AE(NE)+(WS(LEBE+JI)+WS(LEEE-JI))*SINUS

A1(NE)=A1(NE)+(WS(LEB1+JI)+WS(LEE1-JI))*SINUS

A2(NE)=A2(NE)+(WS(LEB2+JI)+WS(LEE2-JI))*SINUS

BE(NE)=BE(NE)+(WS(LEBE+JI)-WS(LEEE-JI))*COSUS

B1(NE)=B1(NE)+(WS(LEB1+JI)-WS(LEE1-JI))*COSUS

B2(NE)=B2(NE)+(WS(LEB2+JI)-WS(LEE2-JI))*COSUS

29 CONTINUE

AE(NE)=AE(NE)+WS(LEME)

A1(NE)=A1(NE)+WS(LEM1)

A2(NE)=A2(NE)+WS(LEM2)

BE(NE)=BE(NE)-WS(LEEE)

B1(NE)=B1(NE)-WS(LEE1)

B2(NE)=B2(NE)-WS(LEE2)

28 CONTINUE

C

C

C

CALCULATE THE HUMAN OPERATORS DESCRIBING FUNCTION AND REMNANT

C

DO 32 K=1,14

DENOM=AE(K)*AE(K)+BE(K)*BE(K)

AR1(K)=SQRT((A1(K)*A1(K)+B1(K)*B1(K))/DENOM)

AR2(K)=SQRT((A2(K)*A2(K)+B2(K)*B2(K))/DENOM)

PHA1(K)=57.3*(ATAN2(B1(K),A1(K))-ATAN2(BE(K),AE(K)))

PHA2(K)=57.3*(ATAN2(B2(K),A2(K))-ATAN2(BE(K),AE(K)))

C

USE THE ASSUMPTION THAT THE HUMANS PHASE LEAD IS LESS THAN

C

180 DEGRESS TO CORRECT FOR THE LOSS OF PHASE INFORMATION

C

IN THE ARC-TANGENT ROUTINES

IF (PHA1(K).LT.180.) GO TO 93

PHA1(K)=PHA1(K)-360.

93 IF (PHA2(K).LT.180.) GO TO 94

PHA2(K)=PHA2(K)-360.

94 CONTINUE

32 CONTINUE

C

C

CONS2 SCALES THE REMNANT

C

CONS2=(DELT)**2/4(PI)T

C

DELT=.02, T=216

CONS2=1.47E-7

DO 33 K=1,15

REM1(K)=CONS2*(AREM1(K)*AREM1(K)+BREM1(K)*BREM1(K))

REM2(K)=CONS2*(AREM2(K)*AREM2(K)+BREM2(K)*BREM2(K))

33 CONTINUE

C

INTERPOLATE FOR THE REMNANT AT THE INPUT FREQUENCIES

DO 230 K=1,14

REMA1(K)=REM1(K)+(REM1(K+1)-REM1(K))*(W(2*K)-W(2*K-1))/(W(2*K+1)-W(2*K-1))

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REMA2(K)=REM2(K)+(REM2(K+1)-REM2(K))*(W(2*K)-W(2*K-1))/(W(2*K+1)-
W(2*K-1))

230 CONTINUE

C CALCULATE THE REMNANT POWER

REMPW1=0.

REMPW2=0.

DO 231 K=1,14

REMPW1=REMPW1+REMA1(K)*(W(2*K-1)-W(2*K+1))

REMPW2=REMPW2+REMA2(K)*(W(2*K-1)-W(2*K+1))

231 CONTINUE

C

C

C WRITE OUT THE FOURIER COEFFICIENTS OF THE SYSTEM ERROR (E), THE
HUMANS OUTPUT (ONE), AND OF THE SYSTEM OUTPUT (TWO).

WRITE(6,100) (K,W(2*K),AE(K),BE(K),A1(K),B1(K),A2(K),B2(K),K=1,14)

C

C WRITE OUT THE FOURIER COEFFICIENTS OF THE REMNANT AT THE HUMANS
OUTPUT (ONE), AND AT THE SYSTEM OUTPUT (TWO).

WRITE(6,101) (K,W(2*K-1),AREM1(K),BREM1(K),AREM2(K),BREM2(K),K=1,1

15)

C

C WRITE OUT THE HUMAN OPERATORS DESCRIBING FUNCTION AND REMNANT AS
WELL AS THE SYSTEM OPEN LOOP DESCRIBING FUNCTION AND REMNANT

WRITE(6,108) (K,W(2*K-1),REM1(K),REM2(K),K=1,15)

WRITE(6,116) CONS2

C WRITE OUT THE HUMANS REMNANT AT THE INPUT FREQUENCIES

WRITE (6,113) (K,W(2*K),REMA1(K),REMA2(K),K=1,14)

C

WRITE(6,103) (K,W(2*K),AR1(K),PHA1(K),AR2(K),PHA2(K),K=1,14)

DO 239 K=1,14

REMA1(K)=REMA1(K)*((1.+AR2(K))**2.)

REMA2(K)=REMA2(K)*((1.+AR2(K))**2.)*(AR1(K)**2.)/(AR2(K)**2.)

239 CONTINUE

WRITE(6,114)

WRITE(6,113) (K,W(2*K),REMA1(K),REMA2(K),K=1,14)

WRITE(6,116) CONS2

C WRITE OUT THE ERROR SCORES

ERRSY=ERRSQ/PUTSQ

ONESY=ONESQ/PUTSQ

TWOSY=TWOSQ/PUTSQ

WRITE(6,107) (PUTSQ,ERRSQ,ERRSY,ONESQ,ONESY,TWOSQ,TWOSY)

WRITE(6,117) X1SQ,X2SQ

PUTSQ=PUTSQ/216.

ERRSQ=ERRSQ/216.

ONESQ=ONESQ/216.

TWOSQ=TWOSQ/216.

WRITE(6,107) (PUTSQ,ERRSQ,ERRSY,ONESQ,ONESY,TWOSQ,TWOSY)

C WRITE OUT THE REMNANT POWER

WRITE(6,112) (REMPW1,REMPW2)

REMPW1=0.

REMPW2=0.

DO 240 K=1,14

REMPW1=REMPW1+REMA1(K)*(W(2*K-1)-W(2*K+1))

REMPW2=REMPW2+REMA2(K)*(W(2*K-1)-W(2*K+1))

240 CONTINUE

WRITE(6,112) (REMPW1,REMPW2)

C SENSE SWITCH 6 DETERMINES WHETHER TO PUNCH OUT THE ANSWERS ON CARDS

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```
C      IF (SENSE SWITCH6) 35,36
C      PUNCH OUT THE DATA ON CARDS, 14 CARDS WITH AR1,PHA1,AR2,PHA2,
C      REMA1, AND REMA2, PLUS 1 CARD WITH PUTSQ,ERRSQ,ONESQ,TWOSQ,
C      REMPW1, AND REMPW2.
35 WRITE(7,115) (AR1(K),PHA1(K),AR2(K),PHA2(K),REMA1(K),REMA2(K),K=1,
114)
      WRITE(7,115) (PUTSQ,ERRSQ,ONESQ,TWOSQ,REMPW1,REMPW2)
36 CONTINUE

C
C
C      THE FOLLOWING STORES EITHER ONE(M) OR TWO(M) ON UNIT 3 FOR
C      LATER PROCESSING FOR THE REMNANT
C      SENSE SWITCH4 DETERMINES WHETHER TO SAVE ONE(M) OR TWO(M)
      IF (SENSE SWITCH4) 95,97
97 REWIND 2
      REWIND 1
      M=1
      N=540
C      THE FOLLOWING AVOIDS THE SPURIOUS DATA POINTS
      DO 521 K=1,3
      CALL BUFFERIN(2,1,TWO(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
521 CONTINUE
      CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      DO 96 K=1,20
      CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      CALL BUFFERIN(2,1,E(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      CALL BUFFERIN(2,1,ONE(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      CALL BUFFERIN(2,1,TWO(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      CALL BUFFEROUT(3,1,PUT(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      CALL BUFFEROUT(3,1,E(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      CALL BUFFEROUT(3,1,ONE(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
      CALL BUFFEROUT(3,1,TWO(M),2*(N-M+1),ISTATUS)
      CALL GOTO(ISTATUS)
96 CONTINUE
95 CONTINUE

C
C
C      RETURN TO INITIALIZE FOR THE NEXT RUN
      GO TO 17
200 STOP

C
C
C      INTERRUPT SUBROUTINE (INTERNAL)
C      INTR SERVICES THE INTERRUPT
C      SUBROUTINE INTR
C
```

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```

C   KRINK IS THE REGISTER COUNTER, 1 TO 1080
    KRINK=KRINK+1
C   KONK IS THE TOTAL COUNTER, 1 ON UP
    KONK=KONK+1
C   KANK IS THE HALF REGISTER COUNTER, 1 TO 500
    KANK=KANK+1
    IF (KONK.GT.1080) GO TO 1
    2 IF (KANK.GE.541) GO TO 3
    4 CALL DAL(0,PUT(KRINK))
12 RETURN
    1 IF (KONK.GT.11880) GO TO 5
    IF (KANK.GE.541) GO TO 6
    8 CALL DAL(0,PUT(KRINK))
    CALL ADL(0,E(KRINK),ONE(KRINK),TWO(KRINK))
C   ADDITIVE PART OF THE FAST FOURIER TRANSFORM
C
C   KL= A COUNTER, 0 TO (2*JA(K)*JC(K)-1)
C   JA=HALF THE NUMBER OF CYCLES PER SECOND/DIVISOR
C   JB=REGISTER START FOR EACH FREQUENCY
C   JC=DIVISOR USED ON HALF THE NUMBER OF SAMPLES PER CYCLE TO GET JA
C
C   ADDITIVE PART OF THE FFT
C
C   ADD THE DATA INTO THE WS(K)
    DO 27 K=1,29
23  KL(K)=KL(K)+1
    JNK=JA(K)*JC(K)
    IF (KL(K).GE.JNK) GO TO 32
    KLE(K)=KL(K)/JC(K) + JB(K)
    GO TO 24
32  JAK=2*JA(K)*JC(K)
    IF (KL(K).GE.JAK) GO TO 33
    KLE(K)=(KL(K)/JC(K))-JA(K)+JB(K)
    GO TO 25
33  KL(K)=-1
    GO TO 23
24  JD=KLE(K)
    JE=KLE(K)+JA(K)
    JF=KLE(K)+2*JA(K)
    WS(JD)=WS(JD)+E(KRINK)
    WS(JE)=WS(JE)+ONE(KRINK)
    WS(JF)=WS(JF)+TWO(KRINK)
    GO TO 26
25  JD=KLE(K)
    JE=KLE(K)+JA(K)
    JF=KLE(K)+2*JA(K)
    WS(JD)=WS(JD)-E(KRINK)
    WS(JE)=WS(JE)-ONE(KRINK)
    WS(JF)=WS(JF)-TWO(KRINK)
26 CONTINUE
27 CONTINUE
    RETURN
    3 KANK=1
    IF (MO.GE.1) GO TO 7
    MO=1
    N=540
    M=1

```

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9 CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)

GO TO 4

7 MO=0

N=1080

M=541

KRINK=1

GO TO 9

6 KANK=1

IF (MO.GE.1) GO TO 10

MO=1

N=540

M=1

11 CALL BUFFERIN(1,1,PUT(M),2*(N-M+1),ISTATUS)

CALL BUFFEROUT(2,1,E(M),2*(N-M+1),ISTATUS)

CALL BUFFEROUT(2,1,ONE(M),2*(N-M+1),ISTATUS)

CALL BUFFEROUT(2,1,TWO(M),2*(N-M+1),ISTATUS)

GO TO 8

10 MO=0

N=1080

M=541

KRINK=1

GO TO 11

5 LOP=1

GO TO 12

C

C

SUBROUTINE GOTO (ISTATUS)

C

SUBROUTINE (INTERNAL) TO HANDLE TAPE READ AND WRITES

7 GO TO (6,4,5,5,5)ISTATUS

6 GO TO 7

5 WRITE (102,200)ISTATUS

4 RETURN

200 FORMAT (\$BUFFERIN STATUS WORD =\$,I2)

END

*LOAD X

*DATA

39.269908

26.179938

19.634954

15.707963

13.089969

8.7266460

7.8539816

6.5449847

5.2359877

4.3633230

3.1415927

2.6179939

2.1816615

1.7453292

1.5707963

1.3089970

1.0471975

.87266462

.72722052

.58177642

.52359877

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.43633231

.34906585

.29088821

.26179938

.17453292

.14544410

.11635528

.08726646

4 1 1

6 13 1

8 31 1

10 55 1

12 85 1

18 121 1

20 175 1

24 235 1

30 307 1

36 397 1

50 505 1

60 655 1

72 835 1

90 1051 1

50 1321 2

50 1651 3

60 1471 2

60 1801 3

54 1981 4

54 2143 5

50 2305 6

60 2455 6

50 2635 9

60 2785 9

60 2965 10

108 3415 10

90 3145 10

90 3739 15

90 4009 20

*FIN

APPLICATION OF A MODIFIED FAST
FOURIER TRANSFORM TO CALCULATE
HUMAN OPERATOR DESCRIBING FUNCTION

By Richard S. Shirley
Electronics Research Center

ABSTRACT

A modified fast Fourier transform (FFT) is used in a hybrid computer program to permit processing of tracking data during a run to yield the human operator's describing function almost immediately after the data-taking period. The computer processing time is substantially reduced at no cost in accuracy.

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